

GTech Surveys Limited

Prestwich Village

Television and Radio Reception Impact Assessment

CHANGE HISTORY

Issue	Date	Details of Changes
0.0	02/10/2023	Working draft
0.1	23/10/2023	First draft issue
1.0	23/11/2023	First issue - minor editing
1.1	07/12/2023	Figure 1 updated. Impact modelling revised as a result of proposed changes to height of Plot G (Travel Hub). Minor editing
1.2	08/12/2023	Description of the Proposed Development updated
1.3	16/01/2024	Red line boundary and description of the Proposed Development updated
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GTech Surveys Limited

GTech Surveys Limited is a Midlands based broadcast and telecommunications consultancy conducting projects throughout the entire UK. We undertake mobile phone network, television and radio reception surveys (pre- and post-construction signal surveys), conduct broadcast interference and reception investigations, and support telecommunications planning work for wind energy developers, construction companies, architects, broadcasters and Local Planning Authorities.

In addition to radio interference modelling services and television reception surveys, we produce EIA and ES Telecommunications Chapters (also known as an 'Electronic Interference Chapter'); satisfying the requirements of Part 5, Regulation 18 (Parts 5a and 5b) of The Town and Country Planning EIA Regulations 2017. We peer review ES and EIA work, liaising with telecommunications providers (Arqiva, BT etc.) and advise developers with respect to associated Section 106 (Town and Country Planning Act 1990) and Section 75 (Town and Country Planning (Scotland) Act 1997) agreements.

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Professional broadcast trained project engineers deliver, and supply QBE insured technical products to support planning applications, discharge planning conditions (including S106 Agreements) and for due diligence. For more information about GTech Surveys Limited please visit our website - www.gtechsurveys.com



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Executive Summary

A signal survey and reception impact assessment have been undertaken to determine the potential effects on the local reception of television and radio broadcast services from the proposed Prestwich Village development. This assessment has been produced to support the planning application submission and to provide the existing reception data to assist with any further studies. Accordingly, impacts to the reception of VHF (FM) radio, digital terrestrial television (DTT also known as Freeview) and digital satellite television services (such as Freesat and Sky), have been assessed. Impacts to the reception of analogue television services have not been assessed in this study because analogue terrestrial television services were switched off in Greater Manchester (Granada TV region) during 2009 and throughout the rest of the UK by 2012.

Due to the existing excellent coverage and lack of receptors in any theoretical signal shadow zone, the Proposed Development is not expected to adversely impact the reception of digital terrestrial television (DTT) services. DTT is commercially known as Freeview.

The Proposed Development is unlikely to cause any interference to the reception of digital satellite television services such as Freesat and Sky.

The Proposed Development is unlikely to adversely impact the reception of VHF(FM) radio broadcasts due to the existing good coverage in the survey area and the technology used to encode and decode radio signals.

Overall, the Proposed Development is unlikely to cause any interference to the reception of any television or radio broadcast platform. As no interference is expected, no mitigation measures are required to restore the optimal reception of any broadcast service. This report provides the existing level and quality of broadcast signal reception in the survey area and can be used to support the planning application submission.

1 - Introduction

This report outlines the findings of a reception impact assessment and pre-construction signal reception survey to determine the viewing preference of receptors located around the proposed Prestwich Village masterplan site and identifies what effects the Proposed Development may have on the reception of television and radio broadcast services.

Prestwich Regeneration LLP is seeking to secure hybrid planning permission for a proposed mixed-use development in Prestwich Town Centre, known as Prestwich Village. This assessment has been prepared by GTech Surveys Limited on behalf of the applicant, Prestwich Regeneration LLP.

The Proposed Development

The Proposed Development consists of a mixed-use development to regenerate the Longfield Centre site within Prestwich Village. A hybrid planning application is proposed to be submitted to Bury Council seeking permission for a mixed-use development. The description of Proposed Development is as follows:

Hybrid application comprising: Full planning application proposing demolition of existing buildings and structures and the erection of a phased mixed use development including a Community Hub comprising flexible uses including library, offices, medical or health services (Use Classes F1 (a-f), F2(b), E(c), E(e), E(g)) and retail uses (Use Classes E(a), E(b) F2(a)) and Sui Generis (hot food takeaway and bar), a new Market Hall (Use Classes E(a), E(b) and Sui Generis (hot food takeaway and bar)), a Commercial Building comprising flexible uses including retail, offices, gymnasium (Use Classes E(a), E(b), E(c), E(d), E(g), F2(a), a Travel Hub comprising car parking and cycle parking (Sui Generis), a public square and public realm and associated landscaping, car parking provision, cycle storage and other associated works; and part Outline planning application (with all matters reserved) proposing a phased residential led mixed use development comprising residential (Use Class C3), flexible commercial, business, service, local community and learning uses (Use Classes E, F) and Sui Generis (hot food takeaway and bar), engineering works to Rectory Lane, new public realm, associated landscaping, car parking provision, cycle storage and other associated works.

The Site

The Site is approximately 2.5 hectares in size and comprises a mixture of surface level car parking and retail units, including the Longfield Centre. The publicly accessible car parking consists of the Fairfax Road Car Park (182 spaces), and the Longfield Centre Car Park (169 spaces). The Site is irregular in shape and bound by Rectory Lane to the east and south; retail units and Bury New Road to the west; and retail units and residential dwellings to the north. Figure 1 shows the location of the application Site.

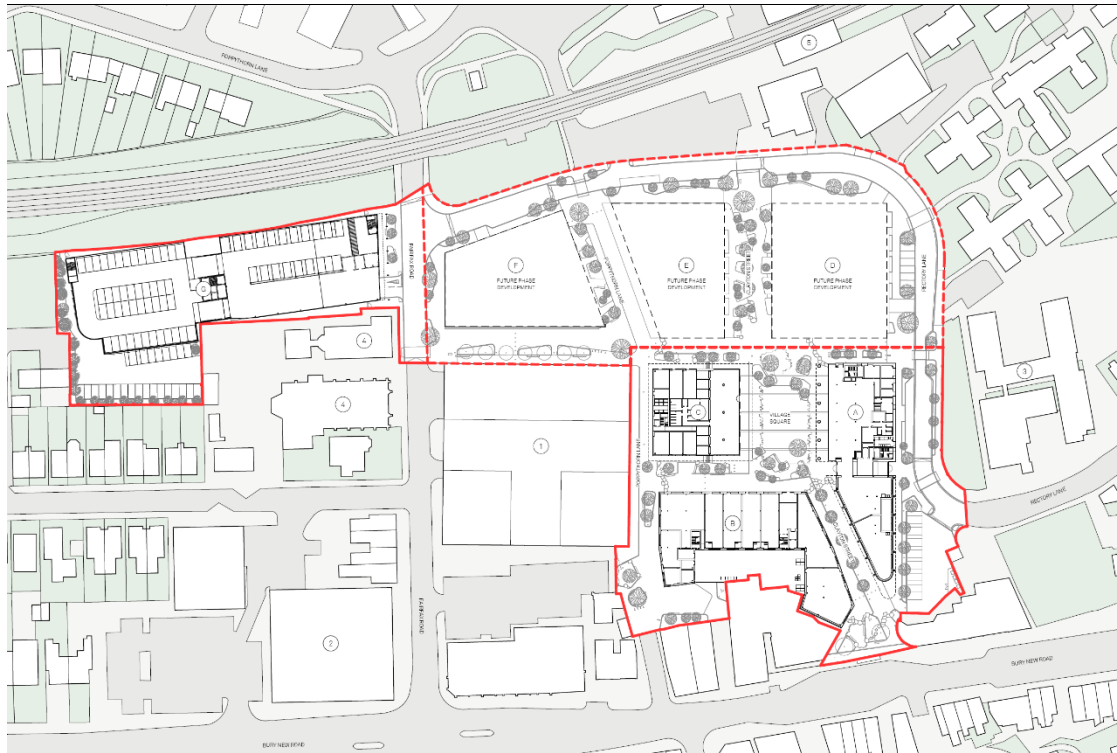


Figure 1 - Location of the Site



The Assessment

To understand the possible impacts and effects upon television and radio reception, a desktop study was first undertaken, based on broadcast transmission information, plans of the Proposed Development and maps of the area. The relevant TV and radio signal survey area for the Proposed Development was identified and a site visit was then subsequently conducted to establish the baseline television reception conditions. Modelling techniques and field assessments of viewers' choice of television and likely radio transmitter were then used to predict the potential effects upon television and radio broadcast reception in the area. The impacts from the Proposed Development are consequently analysed, and together with various mitigation options, conclusions are drawn on the overall effects of the Proposed Development on television and radio broadcast service reception for local residents.

This study was undertaken to investigate whether the Proposed Development could cause interference to local television and radio broadcast reception. The effects on VHF (FM) radio, digital terrestrial television and digital satellite television service reception are discussed. The report also details the baseline reception conditions for future reference. This report follows the following structure:

Chapter 1 introduces the work, the Proposed Development, the site and format of the assessment

Chapter 2 discusses the different forms of structure generated television and radio interference and how these can impact the reception of different television and radio broadcast platforms

Chapter 3 describes the available television and radio services in the survey area

Chapter 4 describes the pre-construction television and radio reception conditions around the Site

Chapter 5 describes the predicted impacts of the Proposed Development upon television and radio broadcast reception before any mitigation measures are applied

Chapter 6 describes any suitable mitigation measures for any affected TV viewer or radio listener

Chapter 7 presents the conclusion

2 - The Mechanisms of Interference to Television and Radio Broadcast Services

Terrestrial Television Services

Any structure will produce two zones of potential disruption to television reception. One zone is where the development creates a 'shadow' (affects all television broadcast platforms) and the other where it gives rise to a 'reflection'. At the frequencies used for broadcasting, the processes of creating a 'shadow' or a 'reflection' are somewhat more complicated than with visible light but thinking of the problem in these terms is still a helpful way of approaching the matter.

Signal 'Shadowing' Effects

In the area behind the structure, the television transmitter is effectively screened from the viewer and the strength of the signal is reduced - Figures 2 and 3.

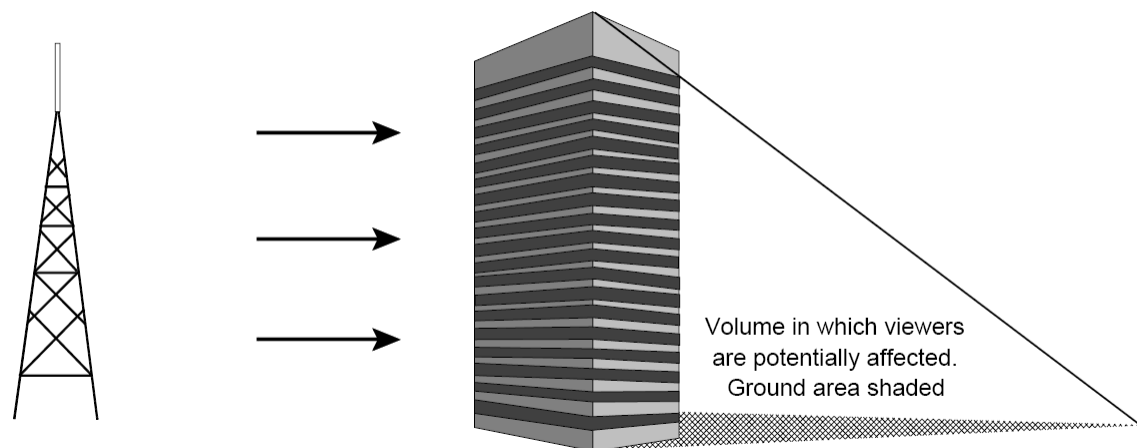


Figure 2 - Affected area in the 'shadow' zone behind the structure

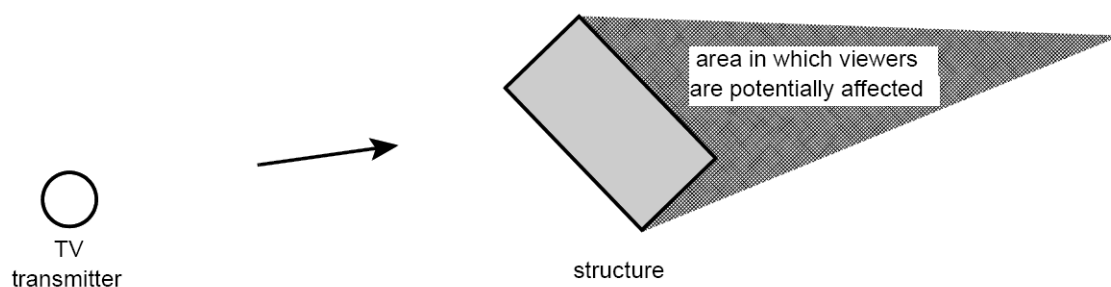


Figure 3 - Plan view of the 'shadow' zone

Television signals do not create such a 'hard' shadow as visible light, and for the purposes of explanation, a 'shadow' zone must be considered which is divided into three sub-zones.

i. Within a few tens of metres from a solid structure, over the region where optical view of the transmitter is lost, the reduction in signal strength is critically dependent on the specific design and composition of the structure. For most brick and concrete buildings, the reduction can be severe and, in some cases, almost total if existing reception conditions are poor.

ii. Further away from the structure (e.g. beyond 25 to 50 metres, but this varies depending on its size) the limit of the 'shadow' zone and signal reduction are determined by diffraction at the edges of the structure and reflection off surrounding structures. The simple condition of whether or not a location has an optical view of the transmitter is not enough to classify the potential interference zone adequately. In general, the effect is that the signal appears to bend around the sides of the structure; the shadow zone reduces in size and the signal strength is reduced by much less than simple ray optics would suggest.

iii. Even further away from the structure (e.g. 250m) complex multiple reflections and diffraction, caused by structures in the locality, may result in the 'shadow' zone becoming almost non-existent, against interfering signals that arrive on significantly different bearings. This can result in an increase in the ratio of wanted to unwanted signal as presented to the television receiver.

Signal 'Reflection' Effects

The second zone of potential interference is produced by 'reflection' or 'scattering' of the incident signal, see Figure 4.

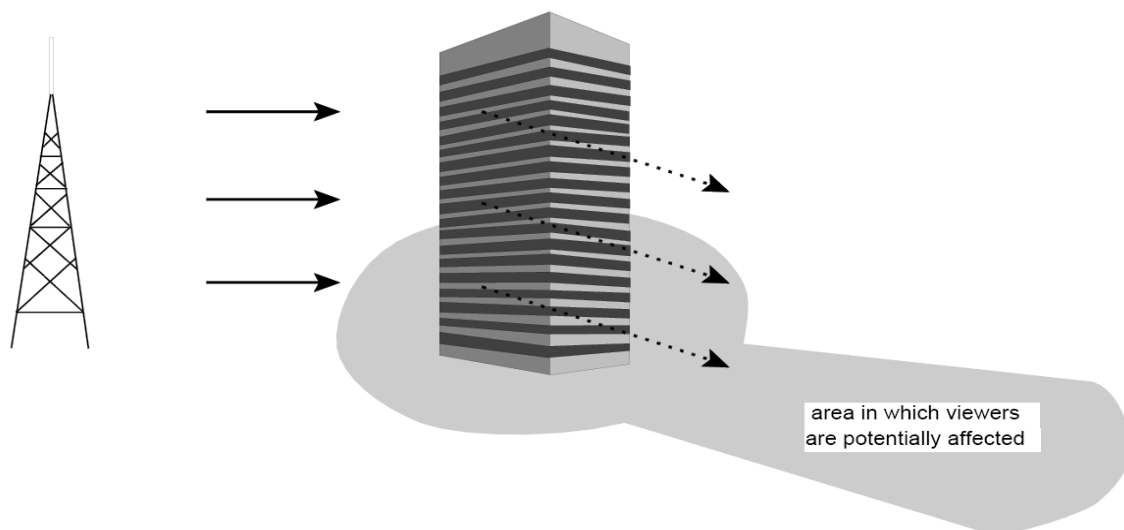


Figure 4 - Affected areas in the 'reflected' zone of the structure

Consider Figure 5, the direct signal travels a distance P1 to the viewer, whilst the signal reflected from the structure travels slightly further, distance (P2 + P3). Although travelling at the speed of light, the different path lengths can mean that one signal arrives with a significant delay relative to the other. This results in a degradation in signal quality.

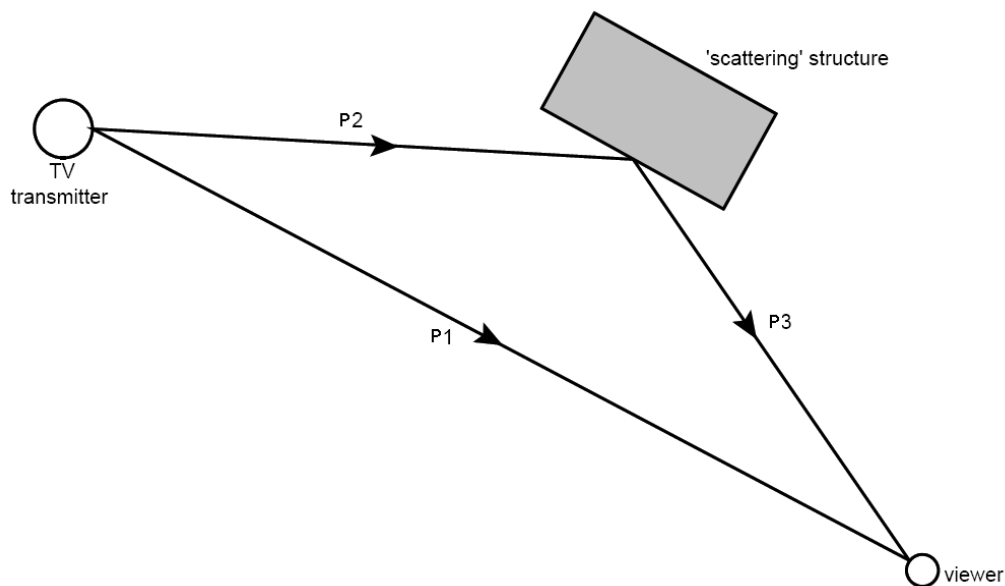


Figure 5 - Direct and Indirect Signal Paths

To avoid interference, it is necessary to ensure that the ratio of wanted signal along the direct path (P1) to the unwanted signal along indirect paths (P2+P3) is sufficiently high. Domestic TV receiving antennas generally have a significant directional response to incoming signals, which means that the antenna may discriminate against interfering signals that arrive on significantly different bearings. This can result in an increase in the ratio of wanted to unwanted signal, as presented to the television receiver.

Digital Terrestrial Television (DTT) - Freeview

The digital television broadcast platform offers many advantages over older analogue broadcast technologies. Due to the way picture signals are encoded and broadcast, digital television offers a much more resilient platform against interference. The construction of digital signals ensures that they are much more impervious to the effects of interference from indirect secondary reflections, which consequently ensures good quality and coherent data stream integrity at the receiver, resulting in an interference free picture. Disruption to DTT services is normally caused by a poor-quality receiving antenna system or locally generated wideband electrical noise. Signal blocking caused by buildings can also degrade received signal quality.

Digital Satellite Television Services - Freesat & Sky

Digital satellite television services are provided by geo-stationary earth orbiting satellites positioned above the equator. To ensure good reception of digital satellite television services, satellite receive antennas (satellite dishes) are normally positioned away from trees and other clutter and are orientated to face the southeastern horizon.

Disruption to digital satellite television services is normally caused by an obstruction on the line-of-sight from the satellite to the receive antenna e.g. a tall building or tall trees. Adverse weather can also influence reception. In the United Kingdom, Freesat and Sky services come from the 28.2 degrees east ASTRA satellite cluster.

Figure 6 below shows typical clearance distances and obstruction heights for interference free satellite television reception.

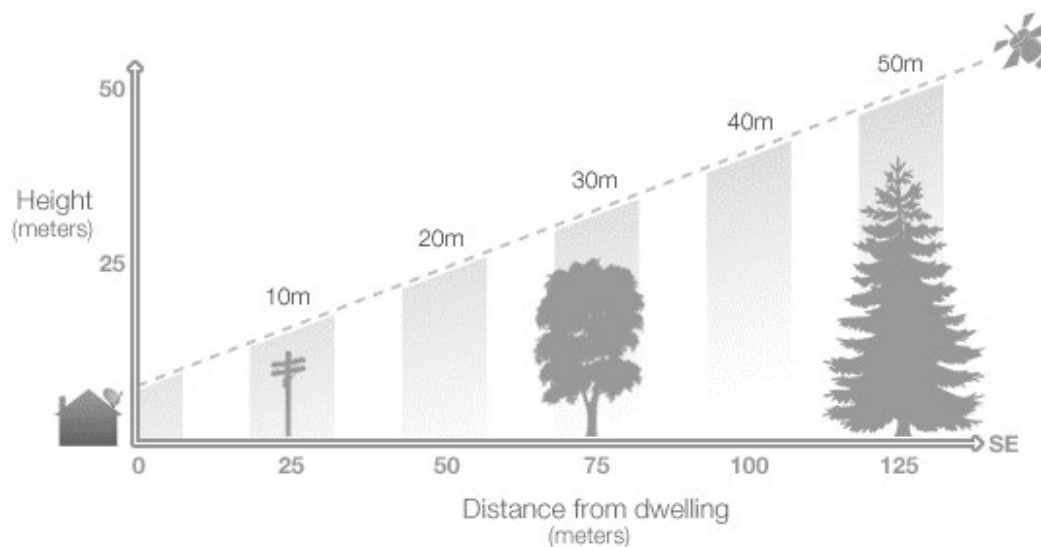


Figure 6 - Typical Clearance Distances and Obstruction Heights for Interference Free Satellite Television Reception

VHF (FM) Radio

VHF (FM) radio services are broadcast from similar structures as terrestrial television services. Many things can cause radio interference, however simple remedies exist that can quickly reduce the effects. Most reception problems on FM radio are caused either by a weak signal or by some kind of interference.

Radio transmission signals will reflect into 'shadow' areas and also reflect from structures to cause 'multi-path' effects. The effect of multiple signals is to create zones of signal cancellation and signal enhancement. This is often demonstrated by the need to carefully position portable radio receivers for good reception or the fluctuation in signal quality whilst listening to VHF (FM) broadcasts in a vehicle. Due to the wavelength of the VHF (FM) signal (at 100 MHz, the wavelength is 3 metres), zones of interference can quickly and easily physically move around, as the interference is generated from the sum interaction of all incoming signals. Consequently, prediction of VHF (FM) interference is not practically possible due to the complex interaction of reflected signals with wanted signals, the design of radio receivers and radio signal propagation characteristics.

Buildings rarely cause radio interference but there is little that can be done during the design stage to reduce any adverse effects. Due to the lower frequencies in use for radio transmission (with respect to television services) and the methods by which the radio signals are encoded, it is very unlikely that a new structure in an already cluttered urban environment will disrupt the reception of radio services.

Non-Terrestrial Television Services (Digital Satellite Television)

For the reception of the 28.2 degrees east ASTRA satellite cluster (Freesat and Sky services), dish elevations of 22.8 degrees are required at this latitude. Optimal receive dish azimuths are 143.8 degrees with respect to true north (approximately southeast).

VHF (FM) Radio

The areas around the Site are served by VHF (FM) radio services of

BBC Radio 1, 2, 3, and 4 from the Holme Moss transmitter (NGR SE 09550 04050)

Technical transmission information for each radio service broadcast from the Holme Moss transmitter are detailed in Table B in the Appendix - *VHF (FM) Radio Transmission Frequencies*.

4 - Survey Methodology & Description of Baseline

Due to the complex nature of television interference in cluttered urban environments, field investigations must be undertaken in the general area around a site to fully evaluate any potential effects. In this study, measurements were undertaken up to one kilometre from the Site, however, the survey mainly focused around the Site and areas to the immediate northwest and southeast, the areas where predicted (modelled) interference could occur. These are identified in Figure 8, and the measurements are detailed in Tables C and D, found in the Appendix - *Signal Measurements*. The following data was recorded:

- Field strength and technical signal measurements of DTT transmissions from the main serving transmitter
- Viewing preference (choice of television transmitter) of residents in all areas visited
- Field strengths of VHF (FM) radio transmissions from the serving transmitter

All television measurements were carried out using a UHF log-periodic receive antenna. VHF (FM) radio field strength measurements were taken with a resonant half wavelength folded dipole antenna at 2 metres AGL, industry standard height for such work. During the survey, no assessment was made of reception conditions within viewers' homes. Equipment details are detailed in the Appendix - *Survey Equipment*.

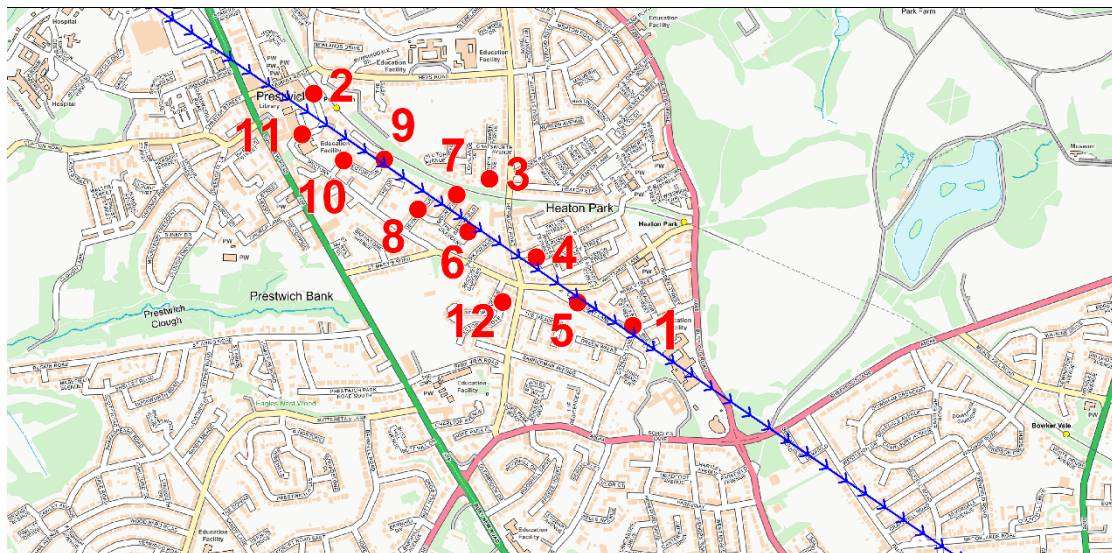


Figure 8 - Surveyed Locations. The blue arrows indicate the direction of the incoming DTT signals from Winter Hill transmitter. The Site is delineated in red

Survey Results and Observations

In general, building use around the Site is mainly for educational, residential, and commercial use. There are a number of medium-rise developments to the immediate northwest of the Site. All terrestrial television antennas observed are directed towards the Winter Hill transmitter.

Digital Terrestrial Television (DTT) - Freeview

A high number of antennas were seen during the survey, due to the typical building use (residential) in the survey area. Additional antennas may also have been mounted on the rooftops of existing tall buildings. DTT services were available at all surveyed locations from the Winter Hill transmitter. At all locations, received signal levels were in excess of recommended minimum amounts and the technical quality of received signals was found to be good². DTT services currently provide very good coverage and service throughout the study area. All terrestrial television antennas observed are directed towards the Winter Hill transmitter.

Digital Satellite Television - Freesat & Sky

Due to the building use within the study area, a high number of few satellite dishes were seen on building sides and rooftops. Additional satellite dishes may have been mounted on rooftops and at the rear of properties; however, these would not be visible from any publicly accessible area. No existing interference has been identified for any satellite television platform.

VHF (FM) Radio

VHF (FM) radio reception conditions were deemed to be good³ throughout the study area. In-car reception was deemed to be good at all locations. This is due to the proximity of the Holme Moss high-power radio transmitter with respect to the Site.

2 - Signal levels as specified by the CAI - Association for Audio Visual Professionals Code of Practice (COP) For the Installation of Aerials/Antennas & Receiving Equipment in the Single Dwelling Unit CAI COP 2: September 2022

Additional technical information regarding the Freeview signal can be found in the Appendix - An Overview of Signal Measurements

3 - Minimum Recommended Field Strengths for Acceptable Levels of VHF (FM) Radio Service

Monophonic audio - 40 dBµV/m
Stereophonic audio (excellent quality) - 54 dBµV/m

Source - https://www.ofcom.org.uk/data/assets/pdf_file/0013/54310/annex-f.pdf

5 - Predicted Impacts and Effects

Methodology

To assess the effects of the Proposed Development upon television and radio broadcast service reception, the structures were considered to create interference to services in the immediate areas around the Site, in signal reflection areas and in the signal shadow zones. These methods, used in conjunction with broadcast transmission information, development plans, maps of the study area and modelling techniques, contribute towards predicting the potential effects upon television and radio broadcast reception in the study area.

The field survey then investigated the areas identified as being at risk of interference and assessed all available services and the transmitter viewing preferences of residents in order to determine if the computed risk is practically valid. The collected data was finally used to determine what actual risks exist and what viable solutions are available to minimise any adverse effects. The predicted effects on television and radio broadcast reception are discussed below and summarised in Table 1.

Digital Terrestrial Television (DTT) - Freeview

Due to the lack of receptors in any theoretical signal shadow areas, and due to the minor changes in massing on the Site with respect to the existing structures on the Site and the new proposed structures, no interference effects are expected. Consequently, no mitigation measures are required to restore optimal reception conditions.

Digital Satellite Television - Freesat and Sky

Tall structures, trees and buildings can disrupt digital satellite television reception by causing obstructions on the line-of-sight to the signal receive dish from the serving satellite. This is discussed further in Chapter 2. Using trigonometry, the approximate maximum height of each proposed building and the angle and orientation of the incoming satellite signals, theoretical signal shadow zones for the 28.2E ASTRA satellite cluster are as indicated;

Element	Max. Signal Shadow Length (m)
Plot A - Community Hub	49
Plot B - Retail Hub	25
Plot C - Market Hall	16
Plot G - Travel Hub	24

These areas extend in a northwesterly direction (323.8 degrees with respect to true north) from the proposed structures' bases. However, as there are no satellite dishes located in any theoretical signal shadow zone, no interference can occur to the reception of digital satellite television services.

VHF (FM) Radio

Modelling VHF (FM) radio interference in a cluttered urban environment is not possible due to the number of constantly changing variables. VHF(FM) broadcast radio reception is robust throughout Prestwich, evident by the survey results and signal availability with a typical car radio. Whilst any new development or structure will change local radio signal propagation and reception characteristics, due to the technical methods involved with encoding and receiving these transmissions, good reception will remain possible. Furthermore, as the reliance on VHF (FM) radio reception decreases due to the uptake of DAB receivers in cars⁴, and online streaming in properties, any possible impact effects are further reduced. Overall, the Proposed Development is not expected to impact the reception of VHF (FM) radio broadcasts.

Broadcast platform	Area(s) of predicted interference	Risk of interference & reasoning	Mitigation
DTT (Freeview)	Non-identified	N/A	Not required
Digital Satellite TV (Freesat and Sky)	Up to 49m to the immediate northwest from the base of the tallest proposed structure (Plot A)	No, because there are no satellite dishes are located in any signal shadow zone	Not required
VHF(FM) Radio	Non-identified	No because coverage is robust	Not required

Table 1 - Summary of Predicted Interference

Predicted Effects - Conclusions

No interference to the reception of DTT (Freeview) services is expected

The Proposed Development is not expected to cause any interference to the reception of digital satellite television services such as Freesat and Sky

The Proposed Development is not expected to affect VHF(FM) radio reception

4 - The Road Vehicles (Approval) Regulations 2020 came into force on 1 September 2020 and has implemented the provisions of the EU Directive covering the compulsory fitment of digital radio in passenger cars and buses that come fitted with a radio.

6 - Mitigation Measures

As no interference to the reception of any television or radio broadcast platform has been identified, no mitigation measures are required to restore broadcast service reception.

7 - Conclusions

A desktop-based study and baseline survey have been performed to assess the possible effects and impacts on the reception of television and radio broadcast services from the proposed Prestwich Village development. The study has focused on the reception of VHF (FM) radio and the two television broadcast platforms that could possibly be impacted by the Proposed Development - digital terrestrial television (DTT) and digital satellite television services.

Digital Terrestrial Television (DTT) - Freeview

Due to existing excellent coverage, robust nature of the DTT signal in the survey area and the spacious massing of the Proposed Development, the Proposed Development is not expected to have any adverse effect upon the reception of Freeview television services.

Digital Satellite Television - Freesat & Sky

Due to lack of viewers (receptors) in any theoretical signal shadow zone and the relatively low height of each element of the Proposed Development, the Proposed Development will not cause any interference to local digital satellite television reception.

VHF(FM) Radio

Due to the existing good coverage and robust technical nature of the broadcast radio network with respect to building-generated signal interference, the Proposed Development is not expected to affect the reception of VHF(FM) radio services.

Overall, the Proposed Development is unlikely to cause any interference to the reception of any television or radio broadcast platform. As no interference is expected, no mitigation measures are required to restore the reception of any broadcast platform. This report details the existing level and quality of radio and television signal reception within the survey area and can be used to support the planning application submission.

APPENDIX

Television Transmission Frequencies

VHF (FM) Radio Transmission Frequencies

Signal Measurements

An Overview of Signal Measurements

Survey Equipment

Calculation of Received Field Strength

References

Mapping Data

Television Transmission Frequencies⁵

Digital TV Multiplex	Multiplex Operator	UHF Channel Number ⁶	Channel Frequency Fc (MHz) ⁷	Transmitter Power (kW)
BBC A	BBC	32	562.00	100.0
D3&4	Digital 3 & 4	34	578.00	100.0
BBC B (HD)	BBC	35	586.00	100.0
SDN	SDN	29	538.00	100.0
Arqiva A	Arqiva	31	554.00	100.0
Arqiva B	Arqiva	37	602.00	100.0

Table A - Winter Hill Digital Terrestrial Television Services

Public Service Broadcaster (PSB) Digital Multiplexes
Commercial (COM) Digital Multiplexes

VHF (FM) Radio Transmission Frequencies

Service	Frequency (MHz)	Transmitter Power (kW)
BBC Radio 1	98.90	250.0
BBC Radio 2	89.30	250.0
BBC Radio 3	91.50	250.0
BBC Radio 4	93.70	250.0

Table B - Holme Moss VHF (FM) Radio Services

⁵ - Information correct at time of writing. Information provided by DigitalUK and Arqiva

⁶ - Digital multiplexes with a "+" or "-" sign operate with a frequency offset making the channel frequency + or - 167 kHz

⁷ - The nominal channel frequency, Fc (in Megahertz) of the multiplex can be calculated using $F_c = 8n + 306$, where 'n' is the UHF channel number

Signal Measurements

Measurement Point Number	Channel Frequency Service	32	34	35	29	31	37
		562.00	578.00	586.00	538.00	554.00	602.00
		BBC A	D3&4	BBC B	SDN	Arqiva A	Arqiva B
1	FS	89.0	89.2	87.2	86.9	88.9	87.8
	CSI	20.8	18.7	-	22.0	21.4	23.7
	MER	30.2	30.6	-	30.4	31.8	31.3
2	FS	87.7	92.7	88.9	92.8	87.5	86.4
	CSI	20.1	18.9	-	17.4	20.3	21.4
	MER	31.5	29.2	-	31.1	31.0	30.9
3	FS	86.9	85.0	89.2	89.3	84.0	84.7
	CSI	20.4	19.0	-	22.3	19.2	18.1
	MER	29.8	32.4	-	31.0	30.2	32.7
4	FS	87.8	82.9	82.9	84.7	87.4	80.9
	CSI	24.3	22.2	-	21.1	21.5	19.0
	MER	30.2	29.9	-	30.5	30.7	31.7
5	FS	86.3	82.7	84.9	86.6	84.4	83.3
	CSI	21.1	22.1	-	20.2	18.9	22.0
	MER	30.3	29.9	-	29.7	29.8	30.7
6	FS	86.4	89.6	87.9	87.0	86.9	96.1
	CSI	21.4	21.4	-	20.5	23.6	23.4
	MER	29.8	31.0	-	30.9	31.4	31.2
7	FS	91.0	89.4	83.4	88.3	88.5	87.0
	CSI	20.4	19.8	-	23.3	23.9	20.3
	MER	30.0	28.6	-	32.4	28.1	29.7
8	FS	91.7	87.7	90.9	91.1	91.7	88.2
	CSI	21.9	21.9	-	23.9	21.2	20.6
	MER	30.3	29.3	-	30.5	28.4	30.4
9	FS	85.8	83.1	83.4	84.5	88.3	83.8
	CSI	20.1	22.0	-	19.4	22.2	22.7
	MER	31.0	30.0	-	29.9	31.7	32.3
10	FS	87.6	82.6	90.3	84.3	86.4	87.7
	CSI	21.0	21.2	-	22.8	21.7	21.0
	MER	29.6	29.6	-	31.3	31.1	29.3

Table C - Winter Hill Digital Television Services

Frequencies listed are in MHz

Field strength (FS) values are indicated in dB μ V/m

CSI Channel Status Information (%)

MER Modulation Error Ratio (dB)

Location	Service	Radio 1	Radio 2	Radio 3	Radio 4
1		61.4	62.6	60.8	63.1
2		63.1	59.8	66.7	67.7
3		62.7	63.7	61.6	61.8
4		63.7	62.3	65.3	59.5
5		58.6	62.0	62.7	59.3
6		61.3	60.8	64.8	62.3
7		61.3	58.8	65.0	61.3
8		60.1	64.4	65.7	61.8
9		63.5	63.0	62.6	59.1
10		59.5	65.2	63.0	59.0
11		61.3	60.8	64.8	62.3
12		61.3	58.8	65.0	61.3

Table D - Field Strength Measurements of Holme Moss VHF(FM) Radio Services

Values are indicated in dB μ V/m

An Overview of Signal Measurements

The first and easiest parameter to check is signal level (also referred to as amplitude or terminated signal strength). In many cases this gives a good indication of the available decoding margin, or the extent of any shortfall.

At the receiver input, the terminated level of a DTT signal is measured in the usual units of dB μ V (a maximum signal level of 70 dB μ V and a minimum signal level of 50 dB μ V). It is helpful to understand that the level of a DTT signal represents the total power of all the carriers in the Coded Orthogonal Frequency Division Multiplexing (COFDM) signal and not the level of each individual COFDM carrier. For satisfactory reception of digital signals, it is important the signals applied to the receiver are within these ranges. These maximum and minimum levels define a so-called window of operation for the receiver.

Common practice dictates that in order to measure the quality of a received DTT signal we have to look at one or more of the following parameters: Bit-Error Rate (BER), Channel BER (CBER), Carrier-to-Noise Ratio (CNR) and Modulation Error Ratio (MER). The Channel State Information (CSI) feature available in DTT measurement equipment is a very valuable tool providing additional insight into the quality of reception in a typical domestic or professional DTT installation.

Using the BER alone is an ill-advised "hit-or-miss" strategy because of the 'cliff-edge effect' characteristic of any digital TV system. A BER reading below the reference quasi error free (QEF) value of 2×10^{-4} might wrongly lead us to conclude that the receiving conditions are satisfactory.

However, the BER provides a very narrow signal measurement range. Even for vanishingly small BER readings, a small drop in the level of received DTT signal can push the DTT receiver over the digital cliff edge beyond the point of system failure. The CBER is closely related to the BER providing a wider signal measurement range. Depending on the type(s) of unknown disturbance(s) affecting our DTT installation (noise, co-channel or adjacent PAL, co-channel DTT, etc.), the CBER corresponding to the reference QEF BER of 2×10^{-4} varies between 4 and 7 in 100. Unfortunately, the CBER is not a reliable indicator of how far the digital cliff edge is.

DTT engineers need a tool with a wide measurement range that solves the shortcomings of the BER and CBER. This measurement tool should provide some estimate of the noise margin of the DTT installation. A first candidate comes to mind: CNR or, alternatively, its sibling the MER.

The CNR is defined as the ratio of the average RF power of the DTT signal to the power of the noise present in the UHF channel. Similarly, the MER is defined as the ratio of the average power of the DTT signal to the average power of the constellation errors. It can therefore be used to give a more direct indication of decoding margin when, as is often the case, there is co-channel

interference as well as noise in the channel. The higher the MER value, the **better** the reception conditions.

In situations where there is no multipath propagation so that the channel frequency response remains reasonably flat, CNR and MER are in principle the same thing. In practice, the accuracy of the measured CNR is limited by the noise floor of the measurement equipment and by the presence of other disturbances on adjacent UHF channels. Likewise, both the receiver's noise floor and other issues resulting from its practical implementation degrade the MER estimate.

Channel State Information (CSI)

Some flavour of CSI is used internally by all commercial DTT receivers to achieve the recommended target system performances⁸. The CSI counts the effect of both the noise present in the channel and the shape of the transmission channel itself. In other words, the CSI gives a measure of the reliability of the received DTT signal. We measure the average of the CSI across the UHF channel occupied by the DTT signal. The higher the percentage value of CSI, the **less** reliable DTT reception is.

As explained, the CSI can be used as a means to measure the noise margin in a DTT installation. Let us call CSI_{QEF} the percentage CSI measured at the point where the measurement equipment displays the reference QEF BER. The noise margin in dB is then approximately given by –

$$NM \text{ (dB)} = \frac{CSI_{QEF} - CSI}{2.6}$$

This empirical approximation represents a good estimate for NM below 8dB. The CSI alone, on the other hand, has a wider measurement range, providing meaningful results for NM of up to 15dB.

⁸ - J. Lago-Fernández, "Using Channel State Information (CSI) to Characterize DVB-T Reception", IBC, Amsterdam, 12-17 September 2002

Survey Equipment

1 x Promax Prolink 4C Premium – Serial Number PK4COPAB11B /
060419030005 Running firmware version 2.47

1 x Sony Wide screen CRT Reference Receiver KV-16TIU – Serial Number
4014480

1 x Professional Broadcast Wideband Log Periodic 8 element antenna
(Amphenol Jaybeam (details below))

**Amphenol JAYBEAM**

468-860 MHz

A Log Periodic antenna designed for UHF Broadcast, TETRA and Cellular communications applications. This antenna is often used in a stacked array to form a rugged, high power, extended range antenna. Produced to the highest quality standards, these robust antenna designs will insure reliable operation in harsh environmental conditions.

Replace "x" with desired model number option.

Electrical Characteristics

Frequency band	468-860 MHz	
Model number options (x)	Model Number LPU/R-N LPU/R-7/16	Connector type N-Female 7/16-DIN Female
Polarization	Vertical or Horizontal	
Horizontal beamwidth	70°	
Gain	7.9 dBd	
Impedance	50Ω	
VSWR	<1.3:1	
Maximum power	250 W	
Connector type	see model number options above	
Lightning protection	DC grounded	

Mechanical Characteristics

Materials	Aluminium Alloy	
Dimensions (Length x Width)	1210 x 320 mm	47.6 x 12.6 in
Weight without bracket	3.5 kg	7.7 lbs

Mounting Options

Mounting	Mounting bracket included to fit 38-50 mm dia. pipe.
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LPU/Rx
V-Pol or H-Pol | Log Periodic | 70° | 7.9 dBd



Technical Specification for an Amphenol Jaybeam Professional Broadcast Wideband Log Periodic 8-Element Antenna

All RF cables, interconnects and systems of professional quality and calibrated to determine feeder losses and antenna gains. These are factored into the results, providing accurate descriptions of actual field strength values – see *Calculation of Received Field Strength*

Calculation of Received Field Strength

The Field Strength (dBμV/m) is derived from the Terminated Level (dBμV) as measured at the input of the measurement receiver.

Field Strength (dBμV/m) = Terminated Level (dBμV) – Aerial Gain (a) + Dipole Factor (b) + Feeder Loss (c)

where -

Dipole Factor (to matched load)	(b)	$20\text{Log}\left(\frac{2\pi}{\lambda}\right)$ <i>Where λ = Transmission Wavelength (m)</i>
Feeder Loss	(c)	3 dB
Aerial Gain (dB _{dipole})	(a)	10 dB

References

The building information found in Chapter 2 was sourced from the following Ofcom documents⁹.

Mapping Data

This report includes mapping and mapping data provided by Ordnance Survey (OS), under the terms of the Open Government Licence, OS data Crown copyright and database copyright (2023).

9 - http://licensing.ofcom.org.uk/binaries/spectrum/fixed-terrestrial-links/wind-farms/tall_structures.pdf

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The UK's terrestrial television and radio networks are highly complex engineering systems and are constantly being modified, re-designed, upgraded and maintained. The reception conditions detailed in this report were those prevailing at the time of the survey in the study area. Engineering work at transmitter sites, weather conditions and the time of the year will influence the quality and coverage of terrestrial services and their susceptibility to interference. Whilst every effort was made to accurately measure and assess the available television and radio transmissions and services at the time of the survey, GTech Surveys Limited cannot assume that any part of the television or radio broadcast network or transmission from any transmitter was operating in required specification or correctly to any design criteria. The signal measurements undertaken during the survey work were used to define the possible impacts to television and radio reception for this project. Although best practice has been applied in understanding the potential impacts, due to the complex nature of the subject, GTech Surveys Limited is not accountable in anyway whatsoever if unpredicted impacts occur at any location anywhere in the study area.

Modelling parameters assume that all installed UHF antenna systems are mounted at least 10m AGL and installed to a modern standard, with all components meeting CAI quality standards. Antennas mounted at lower heights and poor-quality installations will be more prone to the effects of interference from external sources and as such, reception conditions to installations with the aforementioned characteristics have not been accounted for in any impact modelling. Consequently, properties with such installations may be prone to interference effects that have not been identified. Such installations are commonly found in camping and caravan parks, on bungalows and properties where it is not possible to attach an antenna to the exterior roof. Antennas mounted in lofts are also more prone to interference effects arising from the signal attenuation caused by roofing materials. Again, reception conditions to properties with the aforementioned antenna installation characteristics have not been accounted for in any impact modelling and as such, properties with these installations may be prone to interference effects that have not been identified.

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